An Arbitrary Waveform 16 Channel Neural Stimulator with Adaptive Supply Regulator in 0.35 µm HV CMOS for Visual Prosthesis

Jindeok Seo¹, Kyomuk Lim¹, Sangmin Lee², Jaechyun Ahn², Seokjune Hong², Hyungjung Yoo², Sukwon Jung³, Sunkil Park², Dong-il “Dan” Cho², and Hyoungho Ko¹,*

Abstract—We describe a neural stimulator front-end with arbitrary stimulation waveform generator and adaptive supply regulator (ASR) for visual prosthesis. Each pixel circuit generates arbitrary current waveform with 5 bit programmable amplitude. The ASR provides the internal supply voltage regulated to the minimum required voltage for stimulation. The prototype is implemented in 0.35 µm CMOS with HV option and occupies 2.94 mm² including I/Os.

Index Terms—Neural stimulator, adaptive supply regulator (ASR), arbitrary waveform, visual prosthesis

I. INTRODUCTION

Over the past decades, visual prostheses based on functional electrical stimulation (FES) have been brought to great public attention for treating retinal degenerative diseases such as retinitis pigmentosa (RP) and age-related macular degeneration (AMD) [1]. The conceptual diagram of the visual prostheses is shown in Fig. 1. In the retinal structure of RP or AMD patients, the optic nerve is intact, however, the rods and cones are degenerated, thus the neural reaction is not occurred by the external light stimulation. The visual prostheses system using FES can bypass these defects, and can directly stimulate the optic nerve.

FES can be performed by either current or voltage stimulation pulses. Generally the current stimulation method is preferred over the voltage stimulation method in the visual prostheses because the current stimulation can accurately control the delivered amount of charge. The current stimulation, however, can generate quite high electrode voltages that may harm the tissues or damage the electrodes [2].

The current stimulators generally require high output voltage compliance, because the stimulators inject the biphasic current pulse with the maximum amplitude of several hundred µA into the microelectrodes and tissues of several tens kΩ impedance. For example, the output voltage compliance of 10 V (= ±5 V) is required to drive the 10 kΩ with the biphasic current pulse of ±500 µA. Thus, the previous current stimulators are implemented...
using high voltage (HV) CMOS process, and adopt the static high supply voltage of 5 to 35 V [1, 3-6]. Recently, neural stimulator with voltage compliance monitoring circuit for supply adaptation is reported [7], however, the circuit for controlling supply voltage is not included in [7].

The programmability of stimulation waveform is also one of the important issues. While most stimulators use biphasic current-mode rectangular waveforms, the neural researchers discover that the non-rectangular waveforms such as exponential, Gaussian and ramp, and so on, can provide more advanced neural stimulation effect [8]. The previous researches show that different types of applications need different stimulation waveforms in order to produce an optimum stimulation effect [7, 8]. For example, the repeated pulse train was more effective than single pulse stimulation. The asymmetric biphasic pulses have been proven to limit channel interaction between adjacent stimulation sites, and avoid new excitation during the discharge phase. The exponential decrease can reduce the tissue damage. The interphase delay can provide stronger stimulation effects. Recently the neural stimulator with arbitrary programmable pulse shape is reported [8].

This paper proposes a 16 channel arbitrary waveform current stimulator front-end with the adaptive supply voltage regulator (ASR) for the visual prosthesis, as shown in Fig. 2. Each stimulator pixel circuit includes decoding logics, 5 bit digital to analog converter (DAC), biphasic electrode driver and ASR. Each pixel circuits can generate the arbitrary stimulation waveform using the received data packets from global data bus.

In the proposed circuit, the internal power supply voltage is not static, but adaptively regulated to the minimum required voltage for stimulation, thus current stimulation with lower voltage than previous static HV stimulators can be achieved. The ASR provides the adaptively regulated internal supply voltage using current feedback loop. Moreover, the current feedback loop, which monitors the stimulating current and feeds back the monitored current to the regulator, gives the robustness to the variations of the load impedances.

II. SYSTEM DESIGN

1. Top Level Operation

The system consists of the reference circuit, control logic and the 16 channel (4 by 4) stimulator pixel circuit arrays. The each pixel circuit includes digital logic, 5 bit digital to analog converter (DAC) and biphasic current driver with the ASR. The timing diagram of the system is

![Fig. 2. Top-level block diagram of stimulator front-end.](image-url)
2. Current Stimulator with Adaptive Supply Regulator

The schematic of the proposed biphasic current stimulator with ASR is shown in Fig. 4. The operation status of the stimulator is determined by the input signals, STIM_EN, CH_PUSH and BALEN. When STIM_EN is ‘H’, this circuit is activated. The direction of the stimulating current is determined by CH_PUSH. When CH_PUSH is ‘H’, the current flows in forward direction, from channel electrode to reference electrode. When CH_PUSH is ‘L’, the current flows in backward direction, from reference electrode to channel electrode. After the stimulation, the charge balancing, which is to prevent the electrolytic damage by the remaining charge, is enabled by BALEN.

When CH_PUSH = ‘H’, for example, the stimulation current flows through PM2 - channel electrode - retina cell - reference electrode - NM7. If the required output voltage compliance is high, due to the high stimulation current or the large impedance between electrodes, the sourcing current source (PM2) cannot be operated in saturation region, while sourcing current monitor (PM3) is in saturation region. The actual stimulation current of NM7 is monitored by sinking current monitor (NM8), which is in saturation region. In anodic stimulation, \( I_{DS} \) of PM3 and \( I_{DS} \) of NM8 mean the desired current and monitored current, respectively. The current difference, which is the subtraction of the monitored current from desired current, is fed back to the supply regulator. This feedback loop increases the internal supply voltage when the monitored current is smaller than the desired current, and reduces the internal supply voltage when the...
monitored current is higher than the desired current. Thus, the internal supply is adaptively regulated to the minimum required supply voltage using this current feedback loop. Also, the current feedback loop gives the robustness to the variations of the load impedances.

The simulation results of stimulation current variation and adaptive supply voltage with varying load impedance are shown in Fig. 5(a) and Fig. 5(b), respectively. In this simulation, the stimulation current amplitude, AMPL[4:0] is set to “10000”, and the load impedance is increased from 0 Ohm to 20 kOhm. In Fig. 5(a), the stimulation current variation of the ASR stimulator is from +6.75 % to -7.25 %, while the stimulation current variation of the conventional stimulator with static 15 V supply is from +11.30 % to -11.03 % with the load impedance variation from 0 Ohm to 20 kOhm. Fig. 5(b) shows the simulated internal supply voltage of ASR. The internal supply voltage of ASR is increased from 5.6 V to 15 V.

III. PROTOTYPE MEASUREMENTS

The die photograph of the fabricated stimulator chip is shown in Fig. 6(a). The chip is fabricated in 0.35 μm CMOS with HV option and occupies 2.94 mm² including I/O pads. The single pixel circuit consumes 0.12 mm².

With this pixel circuit, 256 channel stimulator can be realized on less than 6 × 6 mm², which is feasible for implantation. The measurement setup is shown in Fig. 6(b). The fabricated chip is directly wire-bonded to the evaluation board (chip-on-board). The stimulation data packets are generated using user interface and data acquisition (DAQ) system.

With the external HV supply of 15 V and load impedance of 10 kΩ, the measured internal supply voltage of ASR and stimulation current is shown in Fig. 7. When the input code of AMPL[4:0] is increased from “00000” to “11111”, the stimulation current is increased from 0 μA to 880 μA, and the adaptive supply voltage is increased from 5.6 V to 15 V.

Fig. 8 shows the measured and simulated stimulation current with varying load impedance. Here, the stimulation current amplitude, AMPL[4:0] is set to “10000”. The measured stimulation current is smaller than simulated current of 22 μA at 10 kOhm load.
impedance. The measured variation of stimulation current is from +8.04 \% to -9.05 \%, while the simulated variation is from +6.75 \% to -7.25 \%, with the load impedance variation of 0 Ohm to 20 kOhm.

Fig. 9 shows the various stimulation current waveforms generated by the fabricated stimulator, which include biphasic square waveforms with interphase delay (Fig. 9(a)), biphasic repeated pulse train waveform (Fig. 9(b)), sinusoidal waveform (Fig. 9(c)), exponential cathodic and anodic waveform (Fig. 9(d)), fast cathodic pulse and slow anodic pulse (Fig. 9(e)), and fast anodic pulse and slow cathodic pulse (Fig. 9(f)).
Table 1. Comparison with previous stimulators

<table>
<thead>
<tr>
<th></th>
<th>[1]</th>
<th>[5]</th>
<th>[6]</th>
<th>[7]</th>
<th>This work</th>
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<tbody>
<tr>
<td># of pixels</td>
<td>256</td>
<td>15</td>
<td>232</td>
<td>2</td>
<td>16</td>
</tr>
<tr>
<td>Static power consumption</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>(Full chip)</td>
<td>1.45 mW</td>
<td>3.2 mW</td>
<td>8 mW</td>
<td>1.16 mW</td>
<td>7.68 mW</td>
</tr>
<tr>
<td>Dynamic power consumption</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>Pattern dependent</td>
<td>Pattern dependent</td>
<td>Pattern dependent</td>
<td>Pattern dependent (max 328.3 mW)</td>
<td></td>
</tr>
<tr>
<td>Stimulation voltage</td>
<td>±12 V</td>
<td>±2.5 V</td>
<td>22.5 V (typ)</td>
<td>35 V (max)</td>
<td>20 V</td>
</tr>
<tr>
<td>Stimulation voltage</td>
<td>Static supply</td>
<td>Static supply</td>
<td>Static supply</td>
<td>Compliance monitor for supply adaption</td>
<td>Adaptive supply regulation</td>
</tr>
<tr>
<td>adaptation</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Process</td>
<td>0.18 µm HV</td>
<td>0.5 µm HV</td>
<td>0.35 µm HV</td>
<td>0.35 µm HV</td>
<td>0.35 µm HV</td>
</tr>
<tr>
<td>Full scale stimulation current</td>
<td>500 µA</td>
<td>960 µA</td>
<td>992 µA</td>
<td>1000 µA</td>
<td>880 µA</td>
</tr>
<tr>
<td>Current DAC Resolution</td>
<td>4 bit</td>
<td>5 bit</td>
<td>5 bit</td>
<td>5 bit</td>
<td>5 bit</td>
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<tr>
<td>Wave-shape programmability</td>
<td>Biphasic rectangular waveform</td>
<td>Biphasic rectangular waveform</td>
<td>Biphasic rectangular waveform</td>
<td>Arbitrary waveform</td>
<td>Arbitrary waveform</td>
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<tr>
<td>Pixel size (mm²)</td>
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<td>N/A</td>
<td>0.1</td>
<td>0.2</td>
<td>0.12</td>
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<tr>
<td>Chip size (mm²)</td>
<td>27.03</td>
<td>5.29</td>
<td>22</td>
<td>N/A</td>
<td>2.94</td>
</tr>
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</table>

The comparison with previous stimulators is given in Table 1. Compared to the previous stimulators, the supply adaptation and wave-shape programmability are main advantage of this work. However, the high static power consumption of 7.68 mW, which is mainly due to the standby current of ASR, is drawback. In the next version of stimulator, the static power consumption will be reduced by adding low power standby mode to ASR.

IV. CONCLUSIONS

A 16 channel, 5 bit controllable arbitrary waveform neural stimulator front-end IC with ASR is developed. Each pixel circuit can generate the stimulation current with programmable wave-shape. The more advanced neural stimulation effect for visual prosthesis can be achieved with this high wave-shape programmability. The internal supply of each pixel is adaptively regulated by ASR. The ASR enables the lower voltage stimulation than conventional static HV supply stimulator when the required voltage compliance is small. Also, the ASR gives the robustness to the variations of the load impedances.

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REFERENCES


**Jindeok Seo** received the B.S. degree in the Department of Electronics from Chungnam National University, Daejeon, Korea, in 2011. Currently, he is pursuing the M.S. degree in the Department of Electronics from Chungnam National University, Daejeon, Korea. His research interests include CMOS biomedical circuit design and analog-to-digital converters.

**Sangmin Lee** received the BS degree in the School of Electrical Engineering and Computer Sciences, Seoul National University, Seoul, Korea, in 2005. Currently he is a PhD candidate student in the School of Electrical Engineering and Computer Sciences, Seoul National University, Seoul, Korea.

**Jae Hyun Ahn** received his B.S. and M.S. degrees in Electrical Engineering from Oklahoma State University, USA in 2000 and 2002 respectively. He was also with Samsung System LSI from 2002 to 2008, where he was involved in the analog front-end design for optical disk products. He is currently working towards his Ph.D. in the School of Electrical Engineering and Computer Science at Seoul National University, Korea.

**Seok-jun Hong** received the B.S. and M.S. degree in Electrical Engineering from Seoul National University, Korea, in 2009 and 2011 respectively. He is currently pursuing the Ph.D. degree in the Department of Electrical Engineering from Seoul National University, Korea. His interests include MEMS fabrication and applications.

**Hyung Jung Yoo** received the BS degree in the School of Electrical Engineering and Computer Science, Kyungpook National University, Daegu, Korea, in 2010 and M.S. degree in the School of Electrical Engineering and Computer Science, Seoul National University, Seoul, Korea, in 2012. Currently he is Ph.D. candidate in the School of Electrical Engineering and Computer Science, Seoul National University, Seoul, Korea.
Suk Won Jung received the B.S. degree and M.S. degree in the Department of Electronics Engineering from the University of Seoul, Korea, in 1994 and 1996, respectively. He is currently pursuing the Ph.D. degree in the Department of Electrical and Computer Science Engineering from Seoul National University, Korea. And he is working for Korea Electronics Technology Institute (KETI) as a managerial researcher. His interests include artificial retinal prosthetic devices, highly sensitivity photonic devices and their application to medical instruments.

Dong-il “Dan” Cho received his BSME degree from Carnegie–Mellon University, Pittsburgh, PA, in 1980 and the M.S. and Ph. D. degrees from Massachusetts Institute of Technology, Cambridge, in 1984 and 1987, respectively. From 1987 to 1993, he was an Assistant Professor in the Mechanical and Aerospace Engineering Department, Princeton University, Princeton, NJ. In 1993, he joined the Department of Control and Instrumentation Engineering, Seoul National University, Seoul, South Korea, where he is currently Professor in the School of Electrical Engineering and Computer Science.

Sunkil Park received his BS degree in mechatronics engineering from Korea University of Technology and Education, Chunan, Korea, in 2003 and M.S. degrees in the School of Electrical Engineering and Computer Science at Seoul National University, Korea, in 2007, respectively. He is currently pursuing the Ph.D. degree in the School of Electrical Engineering and Computer Science at Seoul National University, Korea. His research interest includes the design and fabrication of microactuator and prosthetic devices.

Hyoungho Ko received his BS and Ph. D. degrees in the School of Electrical Engineering from Seoul National University, Korea, in 2003 and 2008, respectively. He was with Samsung Electronics as a senior engineer from 2008 to 2010. In 2010, he joined the Department of Electronics, Chungnam National University, Daejeon, Korea, where he is currently assistant professor. His interests include CMOS analog integrated circuit design.